Special Topics on Residential HVAC

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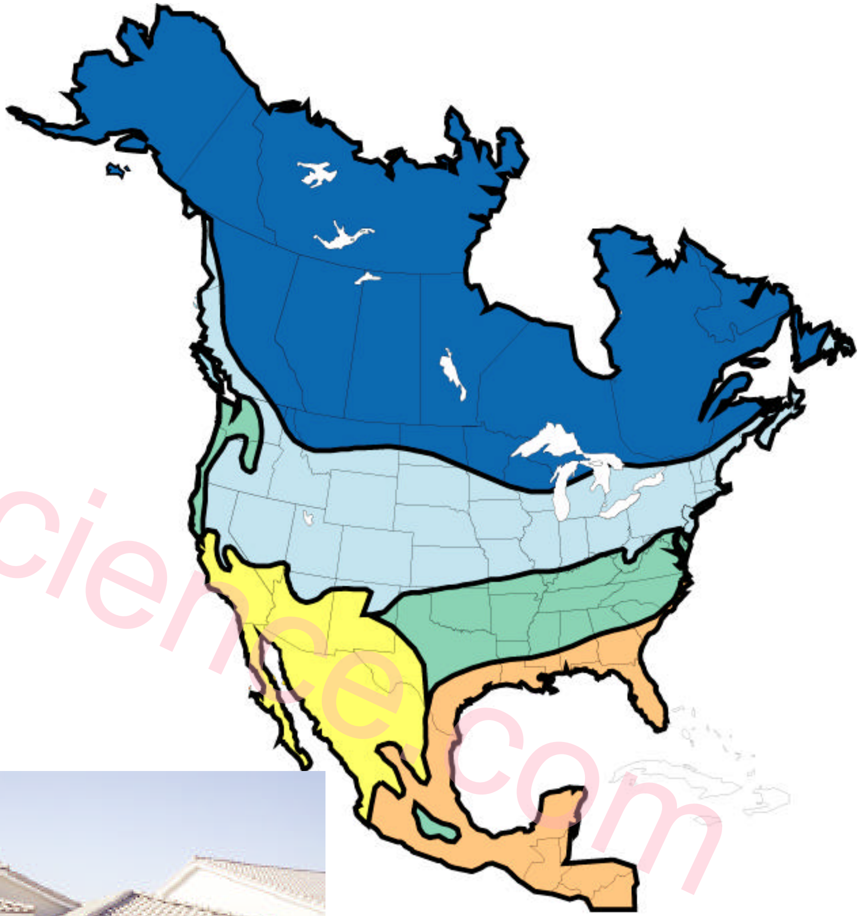
Two Main Topics:

1. ***Cyclical trade-offs between building envelope improvements, reduced system size, and more efficient systems.***

2. ***If I could change two things!***

Climate Specific Design Solutions



Trade-offs

- Better Envelopes
  - Allow for reduced cooling system size
  - Decrease energy consumption
  - Increase occupant comfort
  - Make overall performance more predictable
  - Improve the more permanent features of a home which has longer-term sustainability benefits to society

Trade-offs

- Reduced cooling system size
  - Helps pay for a better envelope
  - Avoids cooling system short-cycling
    - which improves moisture removal
    - allows the system to operate at higher average efficiency

Trade-offs

- More efficient systems
  - Are most cost effective when the load is high
    - this is in conflict with our premise to first reduce loads through improved envelopes
  - High efficiency cooling systems generally have a higher evaporator coil temperature which reduces moisture control
    - this can be changed with effective control of ECM air handlers
  - High efficiency heating systems are generally also sealed combustion which is also good for health and safety

Sealed combustion furnace with ECM air handler and special thermostat

Electronically Commutated Motor (ECM) closeup

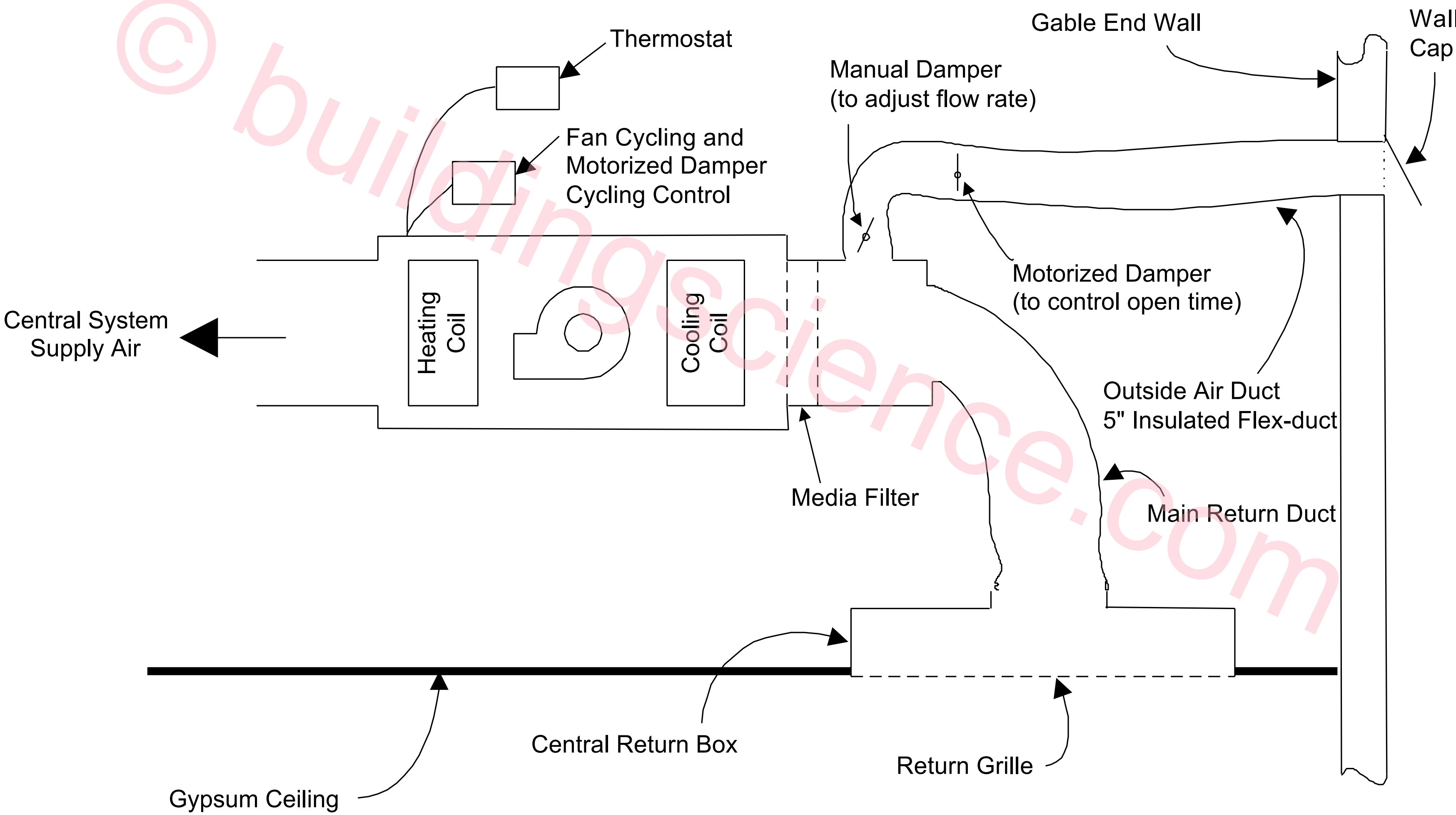
Trade-offs

Let's work with our premise that it's best to improve the envelope first. Where should we start?

- Air distribution system leakage
- Windows
- Random infiltration and controlled mechanical ventilation
- Insulation
  - roofs
  - walls
  - slab-edge (below grade walls)

Central-fan-integrated supply ventilation

Unvented-cathedralized attic configuration
Media filter and motorized damper

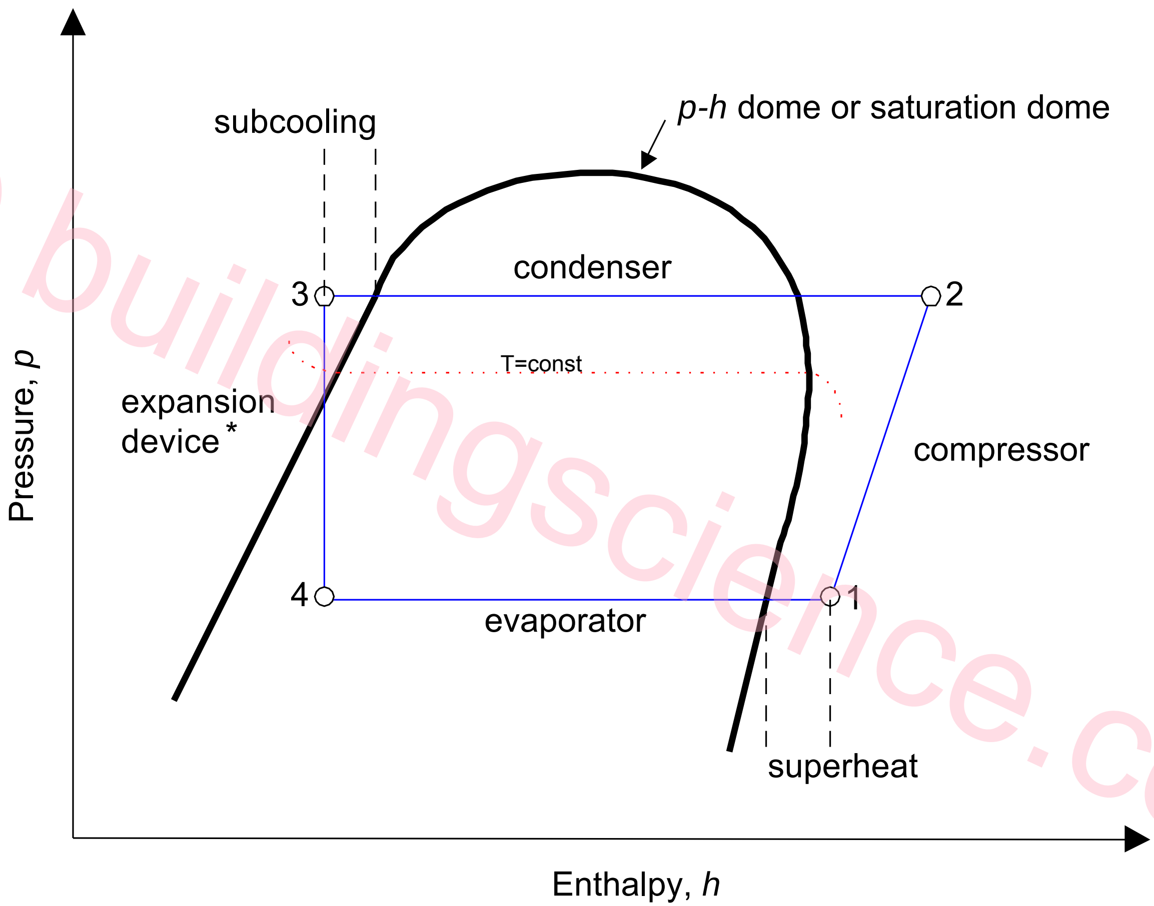


If I could change two things!

#1 All refrigerant cooling systems would have factory installed TXV's

- Thermal expansion valves meter refrigerant to the evaporator and automatically adjust refrigerant flow over a range of system charge and environmental conditions
  - "Super heat controller" protects the compressor from liquid refrigerant
  - Maintains system efficiency under a wide range of operating conditions, precise charging is less important

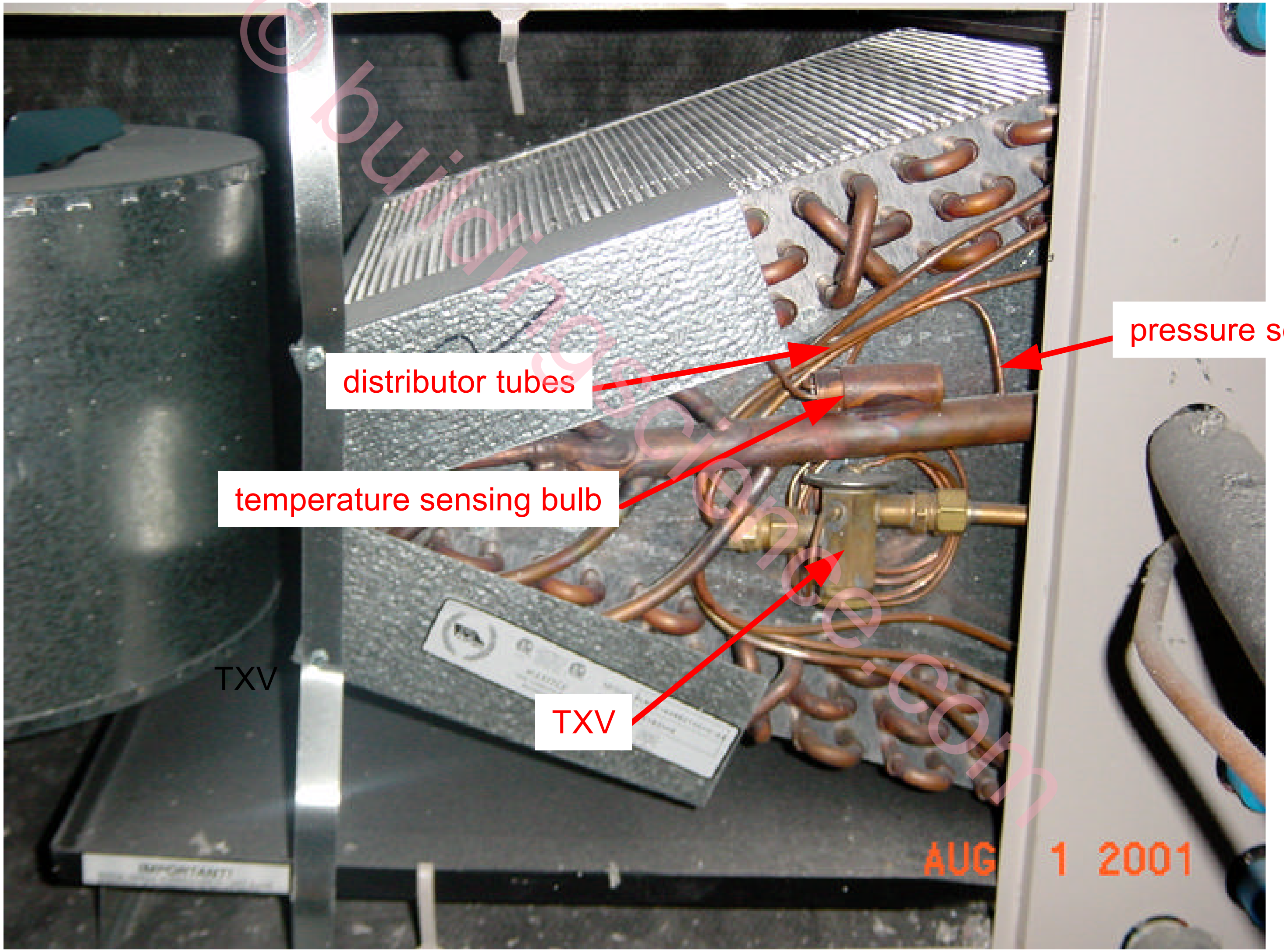
Pressure vs. Enthalpy Diagram
of the Idealized Vapor Compression Refrigeration Cycle



* TXV, fixed orifice, or capillary tube

- Superheat is equal to the vapor line temperature minus the vapor saturation temperature, and is required to make sure that only vapor reaches the compressor
- Subcooling is equal to the liquid saturation temperature minus the liquid line temperature, and is required to make sure that only liquid reaches the expansion device

Thermal expansion valve (TXV) refrigerant metering device



TXV Advantages

- According to research by Proctor Engineering, the performance loss using a TXV metering device is about 5% if the refrigerant charge is off by plus or minus 20%.

- The performance loss using a fixed metering device (capillary tube or orifice) is about 15% to 20% if the refrigerant charge is off by plus or minus 20%.

- According to a California Energy Commision report, installing TXV's in all systems would increase the seasonal efficiency 11%.

What if I think the TXV cost is too high?

Then compare it to the cost of:

- only starting up fixed metering systems when the environmental conditions are favorable to getting a target superheat of 5 F or greater
- waiting a long time while you:
  - add or subtract charge by trial and error
  - let the system settle for 20 minutes before taking new readings and hope the superheat is within 3 F of spec
  - repeat as necessary
  - then often find that the house has cooled down such that your indoor wet bulb temperature is too low to give a target superheat greater than 5 F, so you have to heat the house and start over again (let's hope the gas meter has been set)
- coming back to do this again within the warranty period because of a customer complaint and a slow refrigerant leak

Table 1: Target Superheat (Suction Line Temperature - Evaporator Saturation Temperature)

Condenser Air Dry-Bulb Temperature (°F) ($T_{condenser, db}$)	Return Air Wet-Bulb Temperature (°F) ($T_{return, wb}$)																										
	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76
55	8.8	10.1	11.5	12.8	14.2	15.6	17.1	18.5	20.0	21.5	23.1	24.6	26.2	27.8	29.4	31.0	32.4	33.8	35.1	36.4	37.7	39.0	40.2	41.5	42.7	43.9	45.0
56	8.6	9.9	11.2	12.6	14.0	15.4	16.8	18.2	19.7	21.2	22.7	24.2	25.7	27.3	28.9	30.5	31.8	33.2	34.6	35.9	37.2	38.5	39.7	41.0	42.2	43.4	44.6
57	8.3	9.6	11.0	12.3	13.7	15.1	16.5	17.9	19.4	20.8	22.3	23.8	25.3	26.8	28.3	29.9	31.3	32.6	34.0	35.3	36.7	38.0	39.2	40.5	41.7	43.0	44.2
58	7.9	9.3	10.6	12.0	13.4	14.8	16.2	17.6	19.0	20.4	21.9	23.3	24.8	26.3	27.8	29.3	30.7	32.1	33.5	34.8	36.1	37.5	38.7	40.0	41.3	42.5	43.7
59	7.5	8.9	10.2	11.6	13.0	14.4	15.8	17.2	18.6	20.0	21.4	22.9	24.3	25.7	27.2	28.7	30.1	31.5	32.9	34.3	35.6	36.9	38.3	39.5	40.8	42.1	43.3
60	7.0	8.4	9.8	11.2	12.6	14.0	15.4	16.8	18.2	19.6	21.0	22.4	23.8	25.2	26.6	28.1	29.6	31.0	32.4	33.7	35.1	36.4	37.8	39.1	40.4	41.6	42.9
61	6.5	7.9	9.3	10.7	12.1	13.5	14.9	16.3	17.7	19.1	20.5	21.9	23.3	24.7	26.1	27.5	29.0	30.4	31.8	33.2	34.6	35.9	37.3	38.6	39.9	41.2	42.4
62	6.0	7.4	8.8	10.2	11.7	13.1	14.5	15.9	17.3	18.7	20.1	21.4	22.8	24.2	25.5	27.0	28.4	29.9	31.3	32.7	34.1	35.4	36.8	38.1	39.4	40.7	42.0
63	5.3	6.8	8.3	9.7	11.1	12.6	14.0	15.4	16.8	18.2	19.6	20.9	22.3	23.6	25.0	26.4	27.8	29.3	30.7	32.2	33.6	34.9	36.3	37.7	39.0	40.3	41.6
64	-	6.1	7.6	9.1	10.6	12.0	13.5	14.9	16.3	17.7	19.0	20.4	21.7	23.1	24.4	25.8	27.3	28.7	30.2	31.6	33.0	34.4	35.8	37.2	38.5	39.9	41.2
65	-	5.4	7.0	8.5	10.0	11.5	12.9	14.3	15.8	17.1	18.5	19.9	21.2	22.5	23.8	25.2	26.7	28.2	29.7	31.1	32.5	33.9	35.3	36.7	38.1	39.4	40.8
66	-		6.3	7.8	9.3	10.8	12.3	13.8	15.2	16.6	18.0	19.3	20.7	22.0	23.2	24.6	26.1	27.6	29.1	30.6	32.0	33.4	34.9	36.3	37.6	39.0	40.4
67	-	-	5.5	7.1	8.7	10.2	11.7	13.2	14.6	16.0	17.4	18.8	20.1	21.4	22.7	24.1	25.6	27.1	28.6	30.1	31.5	33.0	34.4	35.8	37.2	38.6	39.9
68	-	-	-	6.3	8.0	9.5	11.1	12.6	14.0	15.5	16.8	18.2	19.5	20.8	22.1	23.5	25.0	26.5	28.0	29.5	31.0	32.5	33.9	35.3	36.8	38.1	39.5
69	-	-	-	5.5	7.2	8.8	10.4	11.9	13.4	14.8	16.3	17.6	19.0	20.3	21.5	22.9	24.4	26.0	27.5	29.0	30.5	32.0	33.4	34.9	36.3	37.7	39.1
70	-	-	-	-	6.4	8.1	9.7	11.2	12.7	14.2	15.7	17.0	18.4	19.7	20.9	22.3	23.9	25.4	27.0	28.5	30.0	31.5	33.0	34.4	35.9	37.3	38.7
71	-	-	-	-	5.6	7.3	8.9	10.5	12.1	13.6	15.0	16.4	17.8	19.1	20.3	21.7	23.3	24.9	26.4	28.0	29.5	31.0	32.5	34.0	35.4	36.9	38.3
72	-	-	-	-	-	6.4	8.1	9.8	11.4	12.9	14.4	15.8	17.2	18.5	19.7	21.2	22.8	24.3	25.9	27.4	29.0	30.5	32.0	33.5	35.0	36.5	37.9
73	-	-	-	-	-	5.6	7.3	9.0	10.7	12.2	13.7	15.2	16.6	17.9	19.2	20.6	22.2	23.8	25.4	26.9	28.5	30.0	31.5	33.1	34.6	36.0	37.5
74	-	-	-	-	-	-	6.5	8.2	9.9	11.5	13.1	14.5	15.9	17.3	18.6	20.0	21.6	23.2	24.8	26.4	28.0	29.5	31.1	32.6	34.1	35.6	37.1
75	-	-	-	-	-	-	5.6	7.4	9.2	10.8	12.4	13.9	15.3	16.7	18.0	19.4	21.1	22.7	24.3	25.9	27.5	29.1	30.6	32.2	33.7	35.2	36.7
76	-	-	-	-	-	-	-	6.6	8.4	10.1	11.7	13.2	14.7	16.1	17.4	18.9	20.5	22.1	23.8	25.4	27.0	28.6	30.1	31.7	33.3	34.8	36.3
77	-	-	-	-	-	-	-	5.7	7.5	9.3	11.0	12.5	14.0	15.4	16.8	18.3	20.0	21.6	23.2	24.9	26.5	28.1	29.7	31.3	32.8	34.4	36.0
78	-	-	-	-	-	-	-	-	6.7	8.5	10.2	11.8	13.4	14.8	16.2	17.7	19.4	21.1	22.7	24.4	26.0	27.6	29.2	30.8	32.4	34.0	35.6
79	-	-	-	-	-	-	-	-	5.9	7.7	9.5	11.1	12.7	14.2	15.6	17.1	18.8	20.5	22.2	23.8	25.5	27.1	28.8	30.4	32.0	33.6	35.2
80	-	-	-	-	-	-	-	-	-	6.9	8.7	10.4	12.0	13.5	15.0	16.6	18.3	20.0	21.7	23.3	25.0	26.7	28.3	29.9	31.6	33.2	34.8
81	-	-	-	-	-	-	-	-	-	6.0	7.9	9.7	11.3	12.9	14.3	16.0	17.7	19.4	21.1	22.8	24.5	26.2	27.9	29.5	31.2	32.8	34.4
82	-	-	-	-	-	-	-	-	-	5.2	7.1	8.9	10.6	12.2	13.7	15.4	17.2	18.9	20.6	22.3	24.0	25.7	27.4	29.1	30.7	32.4	34.0
83	-	-	-	-	-	-	-	-	-	-	6.3	8.2	9.9	11.6	13.1	14.9	16.6	18.4	20.1	21.8	23.5	25.2	26.9	28.6	30.3	32.0	33.7
84	-	-	-	-	-	-	-	-	-	-	5.5	7.4	9.2	10.9	12.5	14.3	16.1	17.8	19.6	21.3	23.0	24.8	26.5	28.2	29.9	31.6	33.3
85	-	-	-	-	-	-	-	-	-	-	-	6.6	8.5	10.3	11.9	13.7	15.5	17.3	19.0	20.8	22.6	24.3	26.0	27.8	29.5	31.2	32.9
86	-	-	-	-	-	-	-	-	-	-	-	5.8	7.8	9.6	11.3	13.2	15.0	16.7	18.5	20.3	22.1	23.8	25.6	27.3	29.1	30.8	32.6
87	-	-	-	-	-	-	-	-	-	-	-	5.0	7.0	8.9	10.6	12.6	14.4	16.2	18.0	19.8	21.6	23.4	25.1	26.9	28.7	30.4	32.2
88	-	-	-	-	-	-	-	-	-	-	-	-	6.3	8.2	10.0	12.0	13.9	15.7	17.5	19.3	21.1	22.9	24.7	26.5	28.3	30.1	31.8
89	-	-	-	-	-	-	-	-	-	-	-	-	5.5	7.5	9.4	11.5	13.3	15.1	17.0	18.8	20.6	22.4	24.3	26.1	27.9	29.7	31.5
90	-	-	-	-	-	-	-	-	-	-	-	-	-	6.8	8.8	10.9	12.8	14.6	16.5	18.3	20.1	22.0	23.8	25.6	27.5	29.3	31.1

source: California Energy Commision report 2001

Phoenix, AZ 1100 ft elev		Maximum outdoor drybulb to use listed minimum indoor wet bulb				
		63	73	84	100	112
		Possibility of 5+ F target superheat at listed minimum indoor wet bulb				
	Indoor, Tdp	50	55	60	65	68
Jan	35	yes	heat to 78	no	no	no
Feb	35	yes	heat to 78	no	no	no
Mar	35	yes	heat to 78	no	no	no
Apr	37	yes	yes	no	no	no
May	38	yes	yes	no	no	no
Jun	44	yes	yes	yes	no	no
Jul	60	n/a	n/a	n/a	yes	heat to 84
Aug	62	n/a	n/a	n/a	yes	heat to 81
Sep	55	n/a	n/a	yes	heat to 83	no
Oct	46	yes	yes	heat to 80	no	no
Nov	38	yes	yes	no	no	no
Dec	35	yes	heat to 78	no	no	no

When it's not more than:

63 F outside, you can check superheat any time (except Jul-Sep when it will never be <63 outside)
73 F outside, it's workable, but requires some pre-heating in winter, and Jul-Sep are out
84 F outside, Jun and Sep are good, Jul-Aug are out, Oct requires pre-heating to 80 F, the rest higher
100 F outside, Jul-Aug are good months, Sep requires pre-heating to 83 F, the rest are out
112 F outside, Jul-Aug require pre-heating to 81 and 84 respectively, the rest are out

Phoenix, AZ 1100 ft elev			Maximum outdoor drybulb to use listed minimum indoor wet bulb				
			63	73	84	100	112
			Minimum indoor drybulb to reach listed minimum indoor wet bulb				
	Outdoor, Tdp	Indoor, Tdp	50	55	60	65	68
Jan	33	35	66	78	91	106	116
Feb	33	35	66	78	91	106	116
Mar	33	35	66	78	91	106	116
Apr	35	37	64	76	89	104	113
May	36	38	63	75	89	103	113
Jun	42	44	57	69	65	97	107
Jul	58	60	--	--	--	75	84
Aug	60	62	--	--	--	71	81
Sep	53	55	--	--	68	83	93
Oct	44	46	55	67	80	95	105
Nov	36	38	63	75	89	103	113
Dec	33	35	66	78	91	106	116

When it's not more than:

- 63 F outside, you can check superheat any time (except Jul-Sep when it will never be <63 outside)
- 73 F outside, it's workable, but requires some pre-heating in winter, and Jul-Sep are out
- 84 F outside, Jun and Sep are good, Jul-Aug are out, Oct requires pre-heating to 80 F, the rest higher
- 100 F outside, Jul-Aug are good months, Sep requires pre-heating to 83 F, the rest are out
- 112 F outside, Jul-Aug require pre-heating to 81 and 84 respectively, the rest are out

If I could change two things!

#2 Get rid of the "caveman" appliances

- Caveman appliances are those that build a fire inside the dwelling and require air from the dwelling to vent combustion products, or don't vent combustion products at all.

Working within the realm of energy-efficient and healthy housing, it can be frustrating to worthless dealing with the various code issues, and the work of verification for:

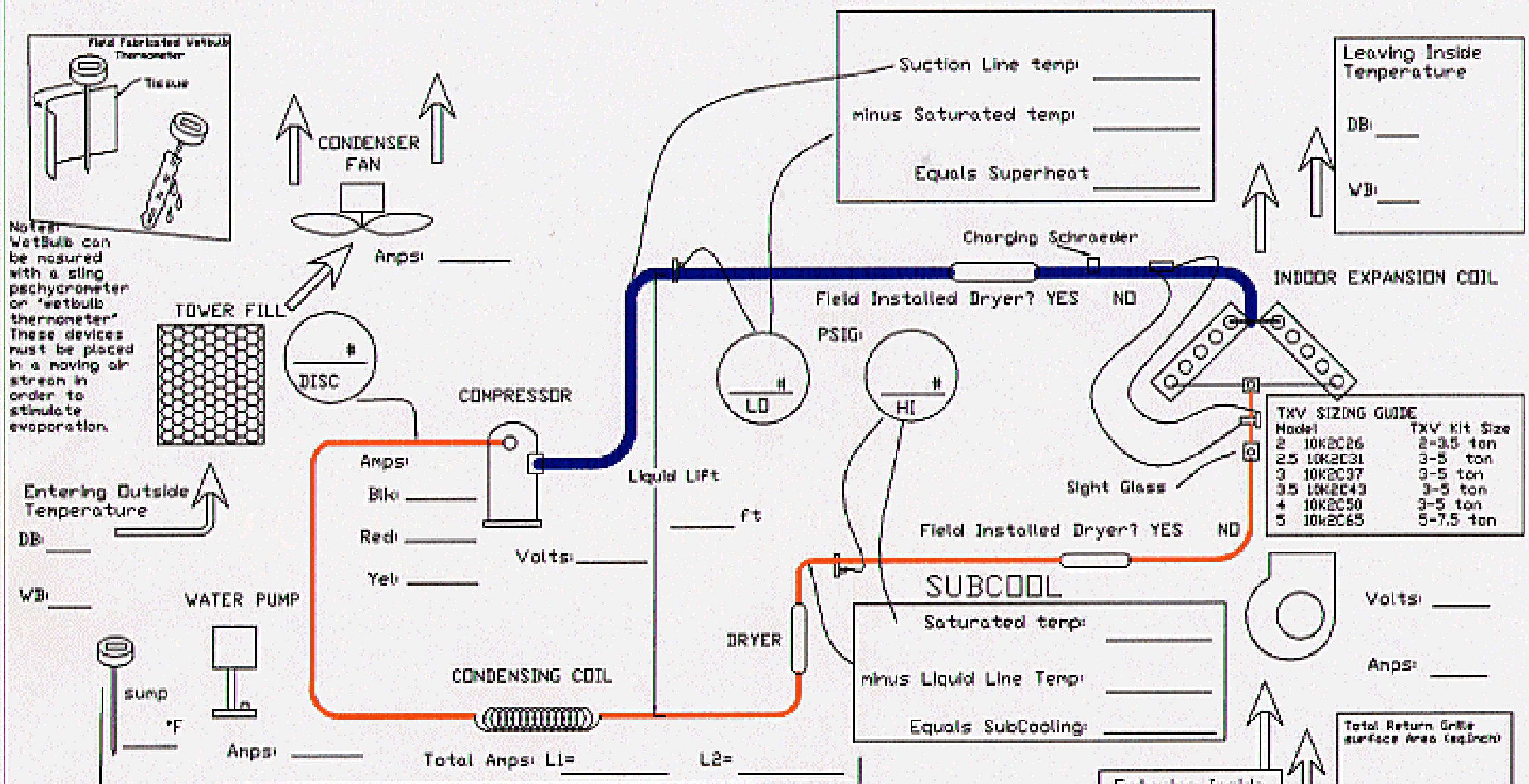
- vent types, sizes, clearances, horizontal distances
- make-up air
- dilution air
- worst case depressurization
- back-drafting

Let’s do--

Sealed combustion only inside conditioned space!

TXV-SUBCOOL OR SIGHT GLASS CHARGING

Site Address	City	State	Phone	Date	Zip



Entering Inside Temperature

DB: ____

WB: ____

Total Return Grille surface Area (sq.inch)

Air Volume Indications
TD<15-HIGH CFM
TD>20-LOW CFM
CHECK AIR FILTER

SUB-COOLING TABLE

Liquid Line Vertical Lift(Ft)	Line Length 0'-25'	Line Length 26'-50'	Line Length 51'-74'
	°F Sub Cooling		
0-10	6	6	6
11-22	6	8	10
23-39	8	11	13
40-50	NA	13	15

NOTES:

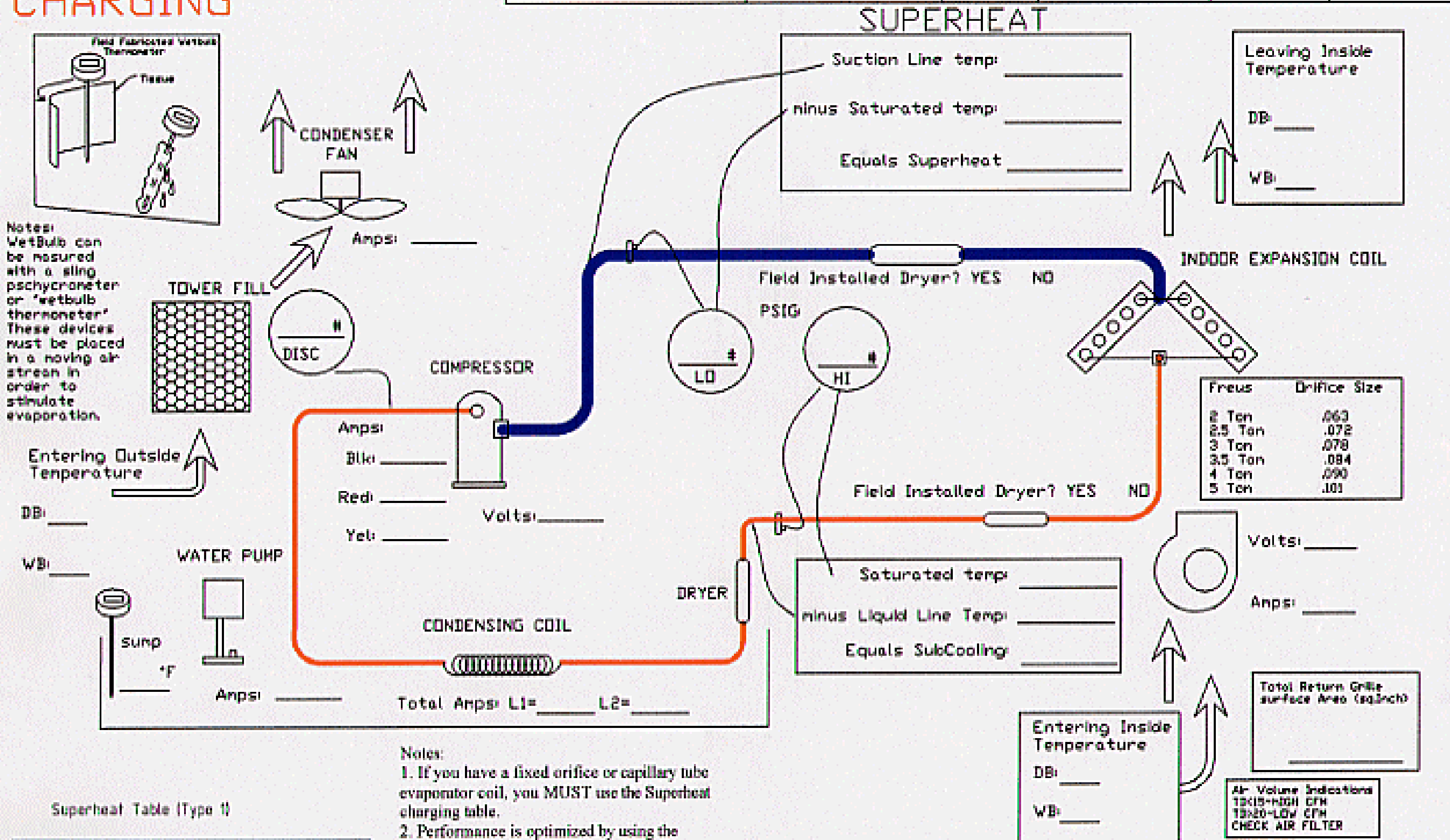
1. TXV systems may be charged either by the subcooling table or by the Sight Glass method.
2. If charging by sight glass, the glass MUST be installed near the evaporator coil, if the line is longer than 25' or has more than 10' of lift.
3. Charging by sight glass- add or recover charge until the sight glass has just barely cleared of bubbles. The system, must be charged enough to clear the glass of bubbles, but overcharging will raise the condensing pressure (after the bubbles have cleared) and lower efficiency. In general, adding charge to raise the condensing pressure (high side) by five pounds after clearing the sight glass allows a good buffer for changing temperature conditions.

Model #:	Serial #:
Coil Model #:	Furnace Model #:

source: Freus Air Conditioning

ORIFICE-SUPERHEAT CHARGING

Site Address	City	State	Phone	Zip	Date



Superheat Table (Type 1)

Ambient Condenser Inlet Temp (°F Wet Bulb)	Indoor Return Air Temperature (°F Dry Bulb)				
	65	70	75	80	85
85	–	2	5	10	12
80	1	3	7	12	15
75	2	4	7	14	18
70	3	5	10	17	20
65	4	5	12	21	26
60	5	10	17	25	29

Notes:

1. If you have a fixed orifice or capillary tube evaporator coil, you MUST use the Superheat charging table.
2. Performance is optimized by using the correct orifice size shown in this chart and charging by the Superheat Table.
3. Within normal operating ranges, an increased orifice size will lower subcooling and may require a reduction in refrigerant charge in order to obtain the recommended superheat.
4. Charging by sight glass in a system that uses a fixed orifice will not work!! Bubbles may appear under normal operating conditions in a fixed orifice system.

Model #: ______ Serial #: ______

Coil Model #: ______ Furnace Model #: ______

source: Freus Air Conditioning

Table 1: Target Superheat (Suction Line Temperature - Evaporator Saturation Temperature) (continued)

		Return Air Wet-Bulb Temperature (°F) ($T_{return, wb}$)																										
		50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76
Condenser Air Dry-Bulb Temperature (°F) ($T_{condenser, db}$)	91	-	-	-	-	-	-	-	-	-	-	-	-	-	6.1	8.1	10.3	12.2	14.1	15.9	17.8	19.7	21.5	23.4	25.2	27.1	28.9	30.8
	92	-	-	-	-	-	-	-	-	-	-	-	-	-	5.4	7.5	9.8	11.7	13.5	15.4	17.3	19.2	21.1	22.9	24.8	26.7	28.5	30.4
	93	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.8	9.2	11.1	13.0	14.9	16.8	18.7	20.6	22.5	24.4	26.3	28.2	30.1
	94	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.2	8.7	10.6	12.5	14.4	16.3	18.2	20.2	22.1	24.0	25.9	27.8	29.7
	95	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.6	8.1	10.0	12.0	13.9	15.8	17.8	19.7	21.6	23.6	25.5	27.4	29.4
	96	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.5	9.5	11.4	13.4	15.3	17.3	19.2	21.2	23.2	25.1	27.1	29.0
	97	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.0	8.9	10.9	12.9	14.9	16.8	18.8	20.8	22.7	24.7	26.7	28.7
	98	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.4	8.4	10.4	12.4	14.4	16.4	18.3	20.3	22.3	24.3	26.3	28.3
	99	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.8	7.9	9.9	11.9	13.9	15.9	17.9	19.9	21.9	24.0	26.0	28.0
	100	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.3	7.3	9.3	11.4	13.4	15.4	17.5	19.5	21.5	23.6	25.6	27.7
	101	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.8	8.8	10.9	12.9	15.0	17.0	19.1	21.1	23.2	25.3	27.3
	102	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.2	8.3	10.4	12.4	14.5	16.6	18.6	20.7	22.8	24.9	27.0
	103	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.7	7.8	9.9	11.9	14.0	16.1	18.2	20.3	22.4	24.5	26.7
	104	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.2	7.2	9.3	11.5	13.6	15.7	17.8	19.9	22.1	24.2	26.3
	105	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.7	8.8	11.0	13.1	15.2	17.4	19.5	21.7	23.8	26.0
	106	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.2	8.3	10.5	12.6	14.8	17.0	19.1	21.3	23.5	25.7
	107	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.7	7.9	10.0	12.2	14.4	16.6	18.7	21.0	23.2	25.4
	108	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.2	7.4	9.5	11.7	13.9	16.1	18.4	20.6	22.8	25.1
	109	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.9	9.1	11.3	13.5	15.7	18.0	20.2	22.5	24.7
	110	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.4	8.6	10.8	13.1	15.3	17.6	19.9	22.1	24.4
	111	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.9	8.1	10.4	12.6	14.9	17.2	19.5	21.8	24.1
	112	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.4	7.6	9.9	12.2	14.5	16.8	19.1	21.5	23.8
	113	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.2	9.5	11.8	14.1	16.4	18.8	21.1	23.5
	114	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.7	9.0	11.4	13.7	16.1	18.4	20.8	23.2
	115	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.2	8.6	10.9	13.3	15.7	18.1	20.5	22.9

source: California Energy Commision report 2001

Table 2: Target Temperature Split (Return Dry-Bulb – Supply Dry-Bulb)

Return Air Dry–Bulb (ºF) ($T_{return, db}$)	Return Air Wet-Bulb (ºF) ($T_{return, wb}$)																										
	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76
70	20.9	20.7	20.6	20.4	20.1	19.9	19.5	19.1	18.7	18.2	17.7	17.2	16.5	15.9	15.2	14.4	13.7	12.8	11.9	11.0	10.0	9.0	7.9	6.8	5.7	4.5	3.2
71	21.4	21.3	21.1	20.9	20.7	20.4	20.1	19.7	19.3	18.8	18.3	17.7	17.1	16.4	15.7	15.0	14.2	13.4	12.5	11.5	10.6	9.5	8.5	7.4	6.2	5.0	3.8
72	21.9	21.8	21.7	21.5	21.2	20.9	20.6	20.2	19.8	19.3	18.8	18.2	17.6	17.0	16.3	15.5	14.7	13.9	13.0	12.1	11.1	10.1	9.0	7.9	6.8	5.6	4.3
73	22.5	22.4	22.2	22.0	21.8	21.5	21.2	20.8	20.3	19.9	19.4	18.8	18.2	17.5	16.8	16.1	15.3	14.4	13.6	12.6	11.7	10.6	9.6	8.5	7.3	6.1	4.8
74	23.0	22.9	22.8	22.6	22.3	22.0	21.7	21.3	20.9	20.4	19.9	19.3	18.7	18.1	17.4	16.6	15.8	15.0	14.1	13.2	12.2	11.2	10.1	9.0	7.8	6.6	5.4
75	23.6	23.5	23.3	23.1	22.9	22.6	22.2	21.9	21.4	21.0	20.4	19.9	19.3	18.6	17.9	17.2	16.4	15.5	14.7	13.7	12.7	11.7	10.7	9.5	8.4	7.2	5.9
76	24.1	24.0	23.9	23.7	23.4	23.1	22.8	22.4	22.0	21.5	21.0	20.4	19.8	19.2	18.5	17.7	16.9	16.1	15.2	14.3	13.3	12.3	11.2	10.1	8.9	7.7	6.5
77	-	24.6	24.4	24.2	24.0	23.7	23.3	22.9	22.5	22.0	21.5	21.0	20.4	19.7	19.0	18.3	17.5	16.6	15.7	14.8	13.8	12.8	11.7	10.6	9.5	8.3	7.0
78	-	-	-	24.7	24.5	24.2	23.9	23.5	23.1	22.6	22.1	21.5	20.9	20.2	19.5	18.8	18.0	17.2	16.3	15.4	14.4	13.4	12.3	11.2	10.0	8.8	7.6
79	-	-	-	-	-	24.8	24.4	24.0	23.6	23.1	22.6	22.1	21.4	20.8	20.1	19.3	18.5	17.7	16.8	15.9	14.9	13.9	12.8	11.7	10.6	9.4	8.1
80	-	-	-	-	-	-	25.0	24.6	24.2	23.7	23.2	22.6	22.0	21.3	20.6	19.9	19.1	18.3	17.4	16.4	15.5	14.4	13.4	12.3	11.1	9.9	8.7
81	-	-	-	-	-	-	-	25.1	24.7	24.2	23.7	23.1	22.5	21.9	21.2	20.4	19.6	18.8	17.9	17.0	16.0	15.0	13.9	12.8	11.7	10.4	9.2
82	-	-	-	-	-	-	-	-	25.2	24.8	24.2	23.7	23.1	22.4	21.7	21.0	20.2	19.3	18.5	17.5	16.6	15.5	14.5	13.4	12.2	11.0	9.7
83	-	-	-	-	-	-	-	-	-	25.3	24.8	24.2	23.6	23.0	22.3	21.5	20.7	19.9	19.0	18.1	17.1	16.1	15.0	13.9	12.7	11.5	10.3
84	-	-	-	-	-	-	-	-	-	25.9	25.3	24.8	24.2	23.5	22.8	22.1	21.3	20.4	19.5	18.6	17.6	16.6	15.6	14.4	13.3	12.1	10.8

source: California Energy Commision report 2001